## TECHNICAL MANUAL HF RECEIVER <br> G133 SERIES



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# G133F HF RECEIVER <br> (PART NO. G133F00000-1) 

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# SECTION I GENERAL DESCRIPTION 

## 1-1. GENERAL

The G133F Receiver is a single-channel SSB-AM$C W$ receiver covering the frequency range between 0.2 mc and 30 mc in 30 bands of 1 -megacycle width each. Twenty-eight positions of the turret plus two positions of overtravel provide the 30 bands. Triple conversion is used for the 0.2 - to 7 -mc bands and double conversion is used for the 7- to $30-\mathrm{mc}$ bands. Audio and i-f outputs are provided.

## 1-2. EQUIPMENT SUPPLIED

| QTY | ITEM | PART NO. |
| :---: | :--- | ---: |
|  |  |  |
| 1 | Receiver | G133F00000-1 |
| As Reqd | Mount | GM19400000-1 |

## 1-3. EQUIPMENT REQUIRED BUT NOT SUPPLIED

| QTY | ITEM | PART NO. |
| :--- | :--- | :--- |
| 1 | Connector | DS07-7S059 |
| 1 | Connector | DS07-7P059 |
| $\mathbf{5}$ | Connector | UG21EU |

## 1-4. ELECTRICAL SPECIFICATIONS

Primary power requirements, signal inputs and outputs, frequency range, bandwidths, and overall system electrical specifications are:

| Type Reception: | SSB-AM-CW |
| :--- | :--- |
| Frequency Range: | 0.2 to 30 mc in 30 one- <br> megacycle bands, continuous <br> coverage |
| Input Power Required:$115-$ or $230-$-volt, single-phase <br> $50-$ to $400-\mathrm{cps}$ ac, 125 watts <br> $(1.09$ amps); 28-volt dc, 4.7 <br> watts (168 milliamperes) |  |
| R-F Input Impedance: | 50 ohms, unbalanced |
| 500-KC I-F Output: | $50-\mathrm{mv}$ minimum into $50-$ ohm <br> load with 5-microvolt <br> input signal |
| Matching Speaker | 4 or 600 ohms |

Line Output Impedance:

Matching Phone Patch Impedance (Local):

Frequency Stability:

Calibration Accuracy:

Audio-Frequency Response: SSB
AM
Audio Output Distortion (SSB Test Signal 100-Microvolt Input, 1.0-W Output):

Local
Line
Q-Multiplier Rejection Notch Depth:

## Receiver Sensitivity

(Nominal):

## AM

SSB and CW

150 ohms unbalanced and 600 ohms balanced.

500 to 600 ohms

During temperature change from 0 to $+50^{\circ} \mathrm{C}$, after 20minute warmup, audio output frequency will not vary more than $\pm 885 \mathrm{cps}$ for carrier frequencies from 2 to 7 mc . From 7 mc to 30 mc , stability varies from 36 PPM $\pm 400$ cps at 7 mc to 27 PPM $\pm 400$ cps at 30 mc . For $\pm 10 \%$ line voltage variation, frequency varies not more than $\pm 100$ cps.

When zeroed to nearest 100kc calibration point, the frequency will be within $\pm 400$ cps.

300 to $2700 \mathrm{cps} \pm 3 \mathrm{db}$
100 to $2500 \mathrm{cps} \pm 6 \mathrm{db}$

Not more than 10 percent Not more than 1.2 percent

Not less than 40 db

3 microvolts for not less than $10-\mathrm{db}$ signal + noise/noise (2 to 30 mc )
15 microvolts for not less than $10-\mathrm{db}$ signal + noise/ noise ( 0.5 to 2 mc )
20.2 microvolts for not less than $10-\mathrm{db}$ signal + noise/ noise ( 0.2 to 0.5 mc )
0.6 microvolts for not less than $10-\mathrm{db}$ carrier on/carrier off ( 2 to 30 mc )
3.0 microvolts for not less than $10-\mathrm{db}$ carrier on/carrier off ( 0.5 to 2 mc )
4.0 microvolts for not less
than $10-\mathrm{db}$ carrier on/carrier off ( 0.2 to 0.5 mc )

Selectivity:
CW (at $6-\mathrm{db}$ points) $300-\mathrm{cps}$ bandwidth
SSB (at 3-db points) 2.4-kc bandwidth
AM (at 6-db points) 5.0-kc bandwidth
Spurious Responses:
Internal Spurious Signals
Other Spurious Responses
Image Response
Less than one microvolt equivalent signal (above 2 mc ) Not less than 80 db down

Not less than 50 db down

## 1-5. MECHANICAL SPECIFICATIONS

Dimensions and weight of the G133F are:

| Dimensions: |  |
| :--- | :--- |
| Height | $6-1 / 4$ inches |
| Width | $18-5 / 16$ (approx) inches. |
| Depth | $12-7 / 8$ (approx) inches. |

Weight:
26 pounds

G133F TUBE AND SEMICONDUCTOR COMPLEMENT

| SYMBOL | TYPE | FUNCTION |
| :---: | :---: | :---: |
| CRI THRU CR4 | IN128 | PRODUCT DEMODULATOR |
| CRS | IN67A | METER RECTIFIER |
| CR6 THRU | 1N1695 | POWER SUPPLY RECTIFIER |
| CR14 | IN482A | AGC RECTIFIER |
| CR15 | IN128 | AM DETECTOR |
| CR16 | 1N482A | AGC STABILIZER |
| CR17 | IN67A | MUTING TRANSIENT SUPPRESSOR |
| CR1201 | INIOOA | MIXER |
| CR1202 | GO2 | ELECTRONIC SWITCH |
| CR1203 | 1N30248 | ZENER REGULATOR |
| Q1 | 2N647 | SSB/CW A-F AMPLIFIER |
| Q1201 | 2 N 1142 | R-F AMPLIFIER |
| Q1202 | 2N1142 | AMPLIFIER |
| Q1203 | 2N1142 | AMPLIFIER |
| Q1204 | 2 N 1142 | AMPLIFIER |
| Q1205 | 2N1142 | IMPEDANCE MATCHING AMPLIFIER |
| V 1 | 6DC6 | R-F AMPLIFIER |
| V2 | 6EA8 | FIRST MIXER AND HF CRYSTAL OSCILLATOR |
| v3 | 6EA8 | SECOND MIXER AND 17.5-MC OSCILLATOR |
| V4 | 6EA8 | THIRD MIXER AND REMOTE GAIN GATE |
| $\begin{aligned} & \text { V5, V7, } \\ & \text { AND V8 } \end{aligned}$ | 6BA6 | I-F AMPLIFIERS |
| V6 | 12AX7 | Q-MULTIPLIER |
| v9 | 6BA6 | AGC AMPLIFIER |
| V10 | 6EA8 | L-F MIXER AND L-F CRYSTAL OSCILLATOR |
| VII | 5670 | I-F CATHODE FOLLOWER AND AGC CATHODE FOLLOWER |
| $\begin{array}{\|l\|l} \mathrm{v} 12 \\ \mathrm{v} 13 \end{array}$ | 6BF5 | SECOND LOCAL A-F AMPLIFIER SECOND LINE A-F AMPLIFIER |
| V14 | 12AX7 | FIRST LINE A-F AMPLIFIER AND FIRST LOCAL A-F AMPLIFIER |
| V15(V501) | 6136 |  |
| V16 | 6EA8 | L-F MIXER AND CALIBRATION OSCILLATOR |
| VI7 V18(V502) | $\begin{aligned} & \text { 6BA6 } \\ & 6136 \end{aligned}$ | BFO <br> VFO AMPLIFIER |

Table 1-1

G133F CRITICAL DIMENSIONS


# SECTION III OPERATION 

## 3-1. GENERAL

The G133F is a single-channel SSB-AM-CW receiver covering a frequency range of 0.2 to 30 megacycles in 30 bands of 1 -megacycle width each. The G133F contains an electronic package which is used to prepare the internal local oscillator signals for processing by external equipment to determine the tuned frequency of the G133F. Both i-f and audio outputs are provided. The audio output level may be visually monitored by a front-panel meter. The meter may also be used to give signal strength indications.

## 3-2. OPERATING CONTROLS

All of the operating controls of the G133F Receiver are located on its front panel. The function of each of the controls is described in the following paragraphs.
a. POWER-- The POWER switch controls the power to the G133F. The positions of this switch are OFF, STBY, ON, and CAL. With the switch in the OFF position, power is removed from the G133F. With the switch in the STBY position, the receiver is disabled but is capable of immediate operation when the POWER switch is put in the ON position. With the switch in the CAL position, the G133F KILOCYCLE dial may be calibrated as explained in paragraph 3-7.
b. RF GAIN -- The RF GAIN control adjusts the gain of the r-f circuits. This control is normally set for the best signal-to-noise ratio in the audio output.
c. MEGACYCLE TUNE -- The MEGACYCLE TUNE control selects the 1 -megacycle band in which the receiver is to operate. The selected frequency band is displayed on the MEGACYCLE counter in the top center of the receiver front panel.
d. KILOCYCLE TUNE-- The KILOCYCLE TUNE control selects the tenth megacycle portion of the operating frequency; the tenth megacycle is displayed on the MEGACYCLE counter. The KJLOCYCLE TUNE control is also used for fine frequency selection. Kilocycles are displayed on the KILOCYCLE dial on the receiver's front panel.
e. ZERO SET -- The ZERO SET control moves the hairline on the KILOCYCLE dial. This control is used to set the zero indication of the KILOCYCLE dial during calibration of the receiver.
f. MODE -- The MODE switch selects the mode of operation of the receiver. Four positions are provided: CW, USB, LSB, and AM.
g. REJECTION TUNING-- The REJECTION

TUNING control provides for suppression of heterodyne interference during AM operation.
h. METER SWITCH -- The METER switch selects the type of signal indication which is displayed on the meter. Three positions are provided: RF, +10DBM, and ODBM. With the meter switch in the RF position, the meter indicates relative signal strength. With the switch in the +10 DBM or ODBM position, the meter indicates the level of the audio output signal.
i. AF GAIN -- The AF GAIN control varies the audio output level.
j. AM BFO ON-OFF SWITCH -- The AM BFO ON-OFF switch in the ON position applies operating power to the beat frequency oscillator. The BFO affects the G133F Receiver in the AM mode only.
k. AM BFO FREQUENCY CONTROL -- The AM BFO FREQUENCY dial, when rotated, varies the BFO frequency from 485 kc to 515 kc . The dial is divided into numbered divisions of $1,2,3$, $4,5,6,7,8,9,0$, and each division is subdivided in increments of 50 providing a total of 500 reset points.

## 3-3. OPERATING PROCEDURES

The following paragraphs outline G133F operation in single-sideband, continuous wave and amplitudemodulated modes. The procedures may vary slightly at the discretion of the operator.

## 3-4. SINGLE-SIDEBAND RECEPTION

When the receiver is to be operated in the singlesideband mode, the following procedures should be used as a guide.
a. Turn the POWER switch to the ON position.
b. Turn the MEGACYCLE TUNE control to obtain an indication on the MEGACYCLE counter corresponding to the desired frequency band.
c. Turn the RF GAIN control fully clockwise.
d. Move the MODE switch to USB for upper sideband reception or to LSB for lower sideband reception.
e. Tune in the desired signal using the KILOCYCLE TUNE control.
f. Set the AF GAIN control for a comfortable listening level.
g. Adjust the KILOCYCLE TUNE control to obtain the most natural sounding audio output.
$h$. Adjust the RF GAIN control to the position which gives the best signal-to-noise ratio.
i. Readjust the AF GAIN control if necessary.

## 3-5. CW RECEPTION

When the receiver is to be operated in the CW mode, the following procedure should be used as a guide.
a. Move the POWER switch to the ON position.
b. Turn the MEGACYCLE TUNE control to obtain an indication on the MEGACYCLE counter corresponding to the desired frequency band.
c. Turn the RF GAIN control fully clockwise.
d. Move the MODE switch to the USB position. If interference is present, move the MODE switch to the $C W$ position for greater selectivity.
e. Tune in the desired signal using the KILOCYCLE TUNE control. If the MODE switch is in the $C W$ position, tune for definite peak in signal strength.
f. Turn the RF GAIN control to approximately midrange, and adjust the AF GAIN control for a comfortable listening level.

## 3-6. AM RECEPTION

When the receiver is to be operated in the AM mode, the following procedure should be used as a guide.
a. Move the POWER switch to the ON position.
b. Turn the MEGACYCLE TUNE control to obtain an indication on the MEGACYCLE counter corresponding to the desired frequency band.
c. Turn the RF GAIN control fully clockwise.
d. Move the MODE switch to the AM position.
e. Tune in the desired signal using the KILOCYCLE TUNE control.
f. Set the AF GAIN control for a comfortable listening level.
g. Adjust the KILOCYCLE TUNE control to obtain the best reception.
h. Adjust the RF GAIN control to obtain the best signal-to-noise ratio.
i. Readjust the AF GAIN control if necessary.

An interfering heterodyne may be suppressed by adjusting the REJECTION TUNING control for minimum interference.


#### Abstract

Note When an interfering signal is present during AM reception, the resulting heterodyne may be suppressed by either of two settings of the REJECTION TUNING control. Select the REJECTION TUNING setting which gives the better intelligibility. The operating range of rotation for the REJECTION TUNING control is 180 degrees. Do not force the control at the OFF position; no OFF position detent will be detected.


If interference or selective fading is present, better reception of AM signals may be obtained by moving the MODE switch to either the USB or LSB position, zero beating the desired carrier, and proceeding according to steps $\mathrm{f}, \mathrm{g}$, and h in paragraph 3-4. Choose the MODE switch position which results in better reception.

## 3-7. CALIBRATION

When the G133F is being calibrated, the following procedure should be used.
a. Move the POWER switch to the CAL position.
b. Move the MODE switch to the USB or LSB position.
c. Turn the KILOCYCLE TUNE control to obtain an indication of 0 kc on the KILOCYCLE dial. (The MEGACYCLE counter and tenth MEGACYCLE counter reading should approximate the desired frequency of operation.)
d. Tune the KILOCYCLE TUNE control to obtain a zero beat.
e. Using the ZERO set knob, move the hairline to 0 on the KILOCYCLE dial.
f. Return the POWER switch to the ON position.

# SECTION IV THEORYOF OPERATION 

## 4-1. GENERAL

The G133F Receiver is shown in block diagram form in figures 4-1 and 4-2. The G133F covers the frequency range from 0.2 to 30 megacycles. Both double-conversion and triple-conversion are used. Triple-conversion is used for the $0.2-\mathrm{mc}$ to $7-\mathrm{mc}$ bands, and double-conversion is used for the $7-\mathrm{mc}$ to $30-\mathrm{mc}$ bands. For $7-\mathrm{mc}$ to $30-\mathrm{mc}$ operation the $14.5-\mathrm{mc}$ to $15.5-\mathrm{mc}$ bandpass network and second mixer are bypassed.

The G133F utilizes a built-in low frequency converter to tune frequencies below 2 mc . The tuning mechanism, counter dials, and turret are arranged so that the two lowest bands, 0.2 to 1 mc and 1 to 2 mc , use the $28-\mathrm{mc}$ to $29-\mathrm{mc}$ and the $29-\mathrm{mc}$ to $30-\mathrm{mc}$ bands of the receiver as a variable i-f (conversion) frequency. As the MEGACYCLE counter is reduced in setting below 2 mc (lowest band on the turret), a segment switch S 6 connects the low frequency converter and its low pass filter between the antenna and the turret input, which is now the $29-\mathrm{mc}$ to $30-\mathrm{mc}$ band. When the MEGACYCLE counter setting is reduced below 1 mc , the segment switch 56 maintains the low frequency converter connection, but the turret is changed to the $28-\mathrm{mc}$ to $29-\mathrm{mc}$ band. In this manner, the 28 positions of the turret plus the two positions of overtravel provide 30 frequency bands, each 1 -megacycle wide. The $0.2-\mathrm{mc}$ limitation of the lowest band is a function of the frequency rolloff in the low pass filter and low frequency losses in the mixer.

The electronic package of the G133F is shown in block diagram form in figure 4-2. This assembly prepares the local oscillator frequencies of the receiver for processing by external equipment to accurately determine the tuned frequency of the G133F. During receiver operation in the first seven frequency ranges ( $0.2-7 \mathrm{mc}$ ), the output of the high frequency crystal-controlled oscillator is mixed with the output of either the $17.5-\mathrm{mc}$ oscillator or the low frequency crystal-controlled oscillator (depending on which one is in use), and the resulting mixed frequency is applied to a notch filter (see figures $4-3$ and 4-4). The notch filter attenuates the basic crystal oscillator frequencies of $8.5,9.5$, and 10.5 mc of the receiver which appear in the mixer output. These frequencies closely approximate the desired output frequency during some receiver operating modes and must therefore be suppressed. The notch filter has lumped constant components which attenuate all frequencies above 9.5 mc so that they will be suppressed in the output. During
operation in the remaining 23 frequency ranges $(7-30 \mathrm{mc})$, the low frequency crystal-controlled oscillator and $17.5-\mathrm{mc}$ oscillator are off, and the output of the high frequency crystal-controlled oscillator goes through the by-pass circuit to the electronic switch. The output of the electronic switch is amplified and applied to output jack J1101 of the electronic package. The output of the variable frequency oscillator, which functions during operation in all 30 bands, is applied through a Darlington amplifier to output jack J 1102 of the electronic package. The outputs of J 1101 ( 3 to 32 mc ) and J1102 ( 2.5 to 3.5 mc ) are routed to external equipment which accurately determines the G133F tuned frequency. The G133F13000-1 Oscillator Assembly provides BFO operation in the AM mode.

## 4-2. DARLINGTON AMPLIFIERS

There are four Darlington amplifiers in the electronic package, one for the output of each receiver oscillator. The Darlington amplifier is a twotransistor, cascaded emitter follower (see figure 7-2). Each amplifier provides more than $60-\mathrm{db}$ decoupling between output and input. Because of the amplifier's low output impedance, the output voltage and waveforms are not affected by cable lengths 25 feet or less. The Carlington amplifiers are encapsulated in epoxy resin to provide protection against moisture, heat, and mechanical damage. The encapsulated circuits are shown in enclosures on the schematic of the electronic package, figure 7-2.

## 4-3. DETAILED THEORY OF OPERATION

A detailed description of the operation of the circuits of the G133F Receiver is given in the following paragraphs. Figure $7-1$ is a schematic diagram of the G133F Receiver.

## 4-4. R-F INPUT TUNING

Signals from the antenna are applied to connector J106 and are routed through switch S6 to imped-ance-matching transformer L30. The output of L30 is coupled to the first section of the double-tuned input network (see figure 4-6). The double-tuned input circuits are composed of capacitors C40 and C71; chokes L33, L32, L31, L69, L68, L67; and the detailed parts mounted on turret wafers A1 through A5. All r-f section detailed parts and turret wafers


## G133D12000-1 ELECTRONIC PACKAGE, BLOCK DIAGRAM



Figure 4-2
G133D12000-1 ELECTRONIC PACKAGE, PARTIAL BLOCK DIAGRAM


Equation: $2 f_{1}-f_{3}-0.5($ Preset $)=f$ signal

# G133D12000-1 ELECTRONIC PACKAGE, PARTIAL BLOCK DIAGRAM 



Figure 4 -4

## G133D12000-1 ELECTRONIC PACKAGE, PARTIAL BLOCK DIAGRAM



Figure 4-5

## R-F INPUT CIRCUITS, SIMPLIFIED SCHEMATIC


are shown in figure 7-3. The first section of this network is tuned by capacitors C40 and Cp and chokes Lp-Lm, L33, L32, and L31. For any position of the turret, L33, L32, L31, and C40 are in the circuit, and the band changing is accomplished by connecting the proper turret-mounted components into the circuit. The tuning slug of $\mathbf{L 3 2}$ is mechanically coupled to the KILOCYCLE TUNE control of the receiver, and the position of the slug is varied to accomplish tuning throughout the megacycle frequency band which is selected by the MEGACYCLE TUNE control. The second section of the network is tuned by capacitors C71 and Cn and chokes Ln-Lm, L69, L68, and L87. The tuning slug of 188 is ganged to the KILOCYCLE TUNE control of the receiver to accomplish tuning in the same manner as that of L32 in the first section of the network. The turretmounted detailed parts are selected by the MEGACYCLE TUNE control. This control positions the turret wafers so that the proper set of detailed parts is connected into the circuit for the desired $1-\mathrm{mc}$ band. Coupling between the two sections of the input network is provided by mutual inductance Lm. The output network consists of a single-tuned circuit using a band-switching and tuning arrangement similar to that of the input network.

## 4-5. FIRST MIXER

The output signal of r-f amplifier V1 is applied to the grid of the first mixer V2A, while the h-f
crystal-controlled oscillator signal is injected at the cathode. The output network consists of a 14.5mc to $15.5-\mathrm{mc}$ bandpass filter for $2-\mathrm{mc}$ to $7-\mathrm{mc}$ operation and a $3-\mathrm{mc}$ to $2-\mathrm{mc}$ variable, tripletuned network for a 7 -mc to $30-\mathrm{mc}$ operation. The slugs of the $3-\mathrm{mc}$ to 2 -mc variable i-f network inductors are mechanically coupled to the KILOCYCLE TUNE control of the receiver and are tracked with the slug-tuned indicators in the r-f circuits to produce the $1-\mathrm{mc}$ coverage for each band.

## 4-6. SECOND MIXER

During $2-\mathrm{mc}$ to $7-\mathrm{mc}$ operation, second mixer V3A uses a $3-\mathrm{mc}$ to $2-\mathrm{mc}$ variable i-f circuit for its output network. This is the same output network that is used by the first mixer during $7-\mathrm{mc}$ to $30-\mathrm{mc}$ operation. The signal from the first mixer plate is passed through the $14.5-\mathrm{mc}$ to $15.5-\mathrm{mc}$ bandpass filter network, T12 and T13, to the grid of the second mixer. The $17.5-\mathrm{mc}$ oscillator signal is injected into the cathode circuit of this mixer. The second mixer is inoperative during $7-\mathrm{mc}$ to $30-\mathrm{mc}$ operation.

## 4-7. THIRD MIXER

The third mixer, V 4 A , receives its input signal from the 3 -mc to 2 -mc variable i-f network. The output signal from the first or second mixer is applied to
the grid of the third mixer, and the VFO signal is injected into the cathode of the third mixer. An external VFO signal may be injected through connector J6 if external frequency control is desired. The third mixer produces the final fixed i-f of 500 kc . Part of the $500-\mathrm{kc}$ i-f signal is applied from the screen of V4A to connector J107. The signal at J107 is suitable for an input to the spectrum display equipment.

The output network of the third mixer is selected by the MODE switch on the front panel. Filter FL2 is used for LSB operation, and filter FL3 is used for USB operation. These are mechanical filters which provide a $2.4-\mathrm{kc}$ bandwidth. The CW position of the MODE switch selects a crystal filter FLA. This crystal filter provides a $300-\mathrm{cps}$ bandwidth. The AM position of the MODE switch selects a network, composed of two loosely-coupled 500-kc i-f transformers T14 and T15, which provides a bandwidth of $5-\mathrm{kc}$.

## 4-8. FIRST I-F AMPLIFIER

The first i-f amplifier V5 receives its input signal from the third mixer through one of the four selective networks described in paragraph 4-7. The output signal is coupled to the Q-multiplier through i-f transformer T1.

## 4-9. Q-MULTIPLIER

The $Q$-multiplier V6 uses a twin triode. The first triode section is a cathode follower, the output of which is coupled to the cathode of the second triode section. When REJECTION TUNING is being used, the signal from the plate of the second triode is coupled through a parallel-tuned circuit to the grid of the second i-f amplifier V7. The parallel-tuned circuit consists of choke L108, capacitors C145 and C146, and a small trimmer capacitor. These parts, plus resistors R33 and R34, form a bridged-T rejection notch filter. The output of the parallel-tuned circuit is also coupled to the grid (pin 7) of the second triode. This feedback arrangement forms a $Q$-multiplier. The $Q$ of L 108 is 250 . The feedback loop has a gain of 10 , resulting in an overall $Q$ of 2500 and a rejection notch depth of not less than $40-\mathrm{db}$. By turning the REJECTION TUNING control fully counterclockwise, the bridged-T network is shorted, deactivating the rejection filter.

## 4-10. SECOND I-F AMPLIFIER

The second i-f amplifier V7 receives its input signal from the $Q$-multiplier network. The output network of the second i-f amplifier is 1-f transformer T2. The secondary of T2 is coupled to the third i-f amplifier V8 and cathode follower V11A.

## 4-11. THIRD I-F AMPLIFIER

The third i-f amplifier V8 receives its input signal from the second i-f amplifier through i-f transformer T2. The third i-f amplifier output is coupled to the product demodulator through i-f transformer T3 and to the AM detector through capacitor C158.

## 4-12. PRODUCT DEMODULATOR

The product demodulator is composed of CR1, CR2, CR3, and CR4 in a diode-ring configuration. The signal from beat-frequency oscillator, V17, is injected into the product demodulator at the junction of resistors R135 and R136. The BFO supplies a reinserted carrier in the place of the carrier missing from the SSB suppressed carrier signal, but the reinserted carrier is cancelled in the product demodulator, leaving only the recovered audio signal in the output. The audio output of the product demodulator is applied to SSB/CW AF preamplifier Q1.

## 4-13. SSB/CW AF PREAMPLIFIER

The output impedance of the product demodulator is approximately 600 ohms. Transistor Q1 provides impedance match and gain between the product demodulator and the following audio amplifier grid circuit. The SSB/CW AF preamplifier is an NPN transistor, connected in a common emitter configuration. Audio signals from the product demodulator and sidetone signals from cathode follower V11B are coupled to the base of Q1. The SSB/CW AF preamplifier output signal is coupled from the collector of Q1 through capacitor C165 to switch S2C. During SSB and CW operation, the contacts of S2C connect the audio output signal to the first local a-f amplifier, V14B, and the first line a-f amplifier, V14A.

## 4-14. AUDIO AMPLIFIER

The audio amplifier of the G133F consists of electron tubes V14A and V13. The first audio amplifier, V14A, receives its input from SSB/CW AF preamplifier Q1 or from AM detector CR15; depending upon the position of MODE switch S2. V14A is a voltage amplifier which drives the second audio amplifier V13. The plate load of V13 is transformer T4, which provides audio output impedances of 150 ohms and 600 ohms. Distortion is reduced by the use of negative feedback from transformer $T 4$ to the cathode of V14A.

## 4-15. LOW FREQUENCY MIXER

For receiving signals in the $0.2-\mathrm{mc}$ to $2-\mathrm{mc}$ range, the G133F uses low frequency mixer V10A and V16A
to convert the signal for reception on the receiver $28-\mathrm{mc}$ and $29-\mathrm{mc}$ bands. The low frequency input to the mixer is passed through a low-pass filter, and the output of the mixer is tuned by the turret and slug-tuned circuits.

## 4-16. OSCILLATORS

Callbration oscillator V16B is a crystal-controlled oscillator operating at 100 rdlocycles. Variable capacitor C227 trims the frequency of the oscillator. The output of the calibration oscillator is coupled to the antenna jack J106. Harmonics of this oscillator will cause beat notes in the audio output at the $100-\mathrm{kc}$ points of the G 133 F tuning range. These beat notes are used for the calibration of the KILOCYCLE dial as outlined in Section III. The calibration oscillator is able to make this calibration only when POWER switch $S 1$ is in the CAL position.

Low frequency crystal-controlled oscillator V10B uses a 14 -me crystal. The plate circuit of this oscillator is tuned to the second harmonic of the crystal. The low frequency crystal-controlled oscillator operates only when G133F is receiving signals in the $0.2-\mathrm{mc}$ to $2-\mathrm{mc}$ bands. The output of this oscillator is coupled to low frequency mixer V16A. Capacitor C2 trims the crystal to frequency.

High frequency crystal-controlled oscillator V2B operates on all bands. The frequency of oscillator operation is determined by one of 16 crystals mounted on a wafer in the turret (see table 4-1). Crystal selection is automatically performed during setting of the MEGACYCLE TUNE control. Individual turret-mounted piston trimmer capacitors trim each crystal to frequency.

The $17.5-\mathrm{mc}$ oscillator, V3B, is crystal controlled. This oscillator operates only when the G133F is operating in the $2-\mathrm{mc}$ to 7 -mc range. Capacitor C233 trims the crystal to frequency.

The variable -frequency oscillator is a Collins 70K4 permeability-tuned oscillator. The frequency of this unit is varied by changing the inductance of L501. This change of inductance is accomplished by turning the KILOCYCLE TUNE knob, which is coupled mechanically to the slug of L501. The output of oscillator tube V15 (V501) is coupled to isolation amplifier V18 (V502). The isolation amplifier is coupled to the cathode of the third mixer through transformer T501.

The beat frequency oscillator (BFO) V17 is a 500 kc crystal-controlled oscillator which operates only when the MODE switch is in USB, LSB, or CW position. The BFO is not for AM operation. Output of the BFO is coupled to the product demodulator.

## 4-17. G133F13000-1 BEAT FREQUENCY OSCILLATOR

The G133F13000-1 Oscillator Assembly, with a fundamental center frequency of 500 kc , operates in the AM mode only. An ON-OFF switch mounted on the receiver front panel is used to connect +28 -volt, d-c power to the oscillator. A helical potentiometer, also mounted on the receiver front panel, is used to vary the oscillator frequency up to a maximum of $\pm 15 \mathrm{kc}$ from the $500-\mathrm{kc}$ center frequency. The potentiometer dial is divided into 10 divisions numbered 1, 2, 3, 4, 5, 6, 7, 8, 9, 0; subdivided into 50 divisions each. Rotating the knob so that the large needle rotates $\pm$ five revolutions from the center setting of the potentiometer constitutes the maximum frequency variation of $\pm 15 \mathrm{kc}$ that is possible. When the AM BFO ON-OFF switch is turned on, the $+28-$ volt, d-c power is supplied to the filter section of the BFO through resistor R1301. Resistor R1302 adjusts the woridng voltage of the BFO frequency potentiometer for the purpose of aligning the center of the potentiometer to coincide with the $500-\mathrm{kc}$ i-f center frequency of the receiver. Variable capacitor C1307 is used to adjust the resonant frequency of the tank circuit to assure that the center frequency of the BFO is at the desired $500-\mathrm{kc}$ setting prior to adjustment of R1302. The potentiometer varies the voltage to the variactors CR1302 and CR1303 that are across the tank circuit comprised of coil L1301, capacitor C1304, and variable capacitor C1307. The capacitance of the variactors varies with the amount of the bias voltage applied to the variactors. Varying the capacitance of the variactors varies the resonant frequency of the tank circuit from the 500 -kc center frequency. The output of the tank circuit is applied to the oscillator transistor Q1301. Resistor R1307 decreases the Q of the tank circuit comprised of coil L1304 and capacitor C1309 that is used to develop a feedback voltage to the oscillator through capacitor C1305. The tank circuit comprised of coil L 1305 and capacitor C1311 is used as a harmonic suppressor for all harmonics and allows only the fundamental frequency at the BFO output to be applied to the AM detector of the receiver. The tank circuit comprised of coil L1303 and capacitor C1308 forms a decoupling network which is connected to the AM position of the receiver mode switch. When the receiver mode switch is placed in the AM position, the BFO decoupling network is connected to ground. This furnishes a d-c path to the emitter of transistor Q1301 permitting operation of the oscillator. This assures that the BFO operates only in the AM mode.

## 4-18. SPECIAL CIRCUITS

Cathode follower V11A receives i-f excitation from the second i-f amplifier. The output of this cathode
follower is applied to automatic gain control (AGC) amplifier V9. Output of the AGC amplifier is coupled to the AGC rectifier CR14 and through the lowpass filter to the i-f output connector J105.

AGC rectifier CR14 rectifies the i-f signal from the AGC amplifier V9. The d-c output from the AGC rectifier is used for automatic gain control of the $r-1$ and $1-f$ amplifiers.

The sidetone output of an associated system transmitter may be connected to connector J8. This allows audible monitoring of transmission. The sidetone signal is applied to cathode follower V11B. The output of V11B is applied to SSB/CW/AF preamplifier Q1 and then to the audio amplifier.

Diode CR16 in the grid return circuit of r-i amplifier V1 is used to stabilize the AGC circuit by preventing oscillatory action in the AGC loop.

Dlode CR17 stabilizes the r-f gain control bus by suppressing transients which occur during mute on-off switching.

Remote gain gate V4B presents a high-impedance isolation between the remote gain line and the AGC circuit. This prevents the low-impedance remote gain circuit and the bias supply from loading the high-impedance AGC circuits.

## 4-19. G133D12000-1 ELECTRONIC PACKAGE

A detalled description of the operation of the circuits of the electronics package is given in the following paragraphs. Figure $7-2$ is a schematic diagram of the electronics package.

## 4-20. OPERATION IN THE O.2-TO 2.0-MC TUNING RANGE

During operation in the $0.2-$ to $2.0-\mathrm{mc}$ range, both the low frequency crystal-controlled oscillator and the high frequency crystal-controlled oscillator are operating (see figures 4-3, 7-1, and 7-2). The output of the low frequency oscillator is applied through J1104 of the electronic package to Darlington amplifier A1203, which provides $60-\mathrm{db}$ decoupling between the oscillator and amplifier Q1201. The high frequency oscillator signal is applied through J1103 of the electronics package to Darlington amplifier A1201, which provides $60-\mathrm{db}$ decoupling between the oscillator and amplifier Q1201. The high frequency output of A1201 and the $28-\mathrm{mc}$ output of A1203 are linearly mixed in the base circuit and then amplified by Q1201.

When the low frequency oscillator is operating, a $\mathrm{B}+$ voltage is applied through C1106 and R1226 to the anode of CR1202. This positive voltage forward
biases CR1202, preventing the output of Q1201 from being coupled to Q1203 through C1206, C1207, and R1216; C1209 and R1219, C1211, and C1220. When CR1202 is forward biased, the output of C1207 is shorted to ground.

The output of Q1201 is coupled through C1202 to CR1201 which rectifies the signal. This rectified signal is applied to amplifier Q1202. Q1202 amplifies the signal to help overcome the loss in the following filters. The LC filter (consisting of L1202 through L1204, C1210, and C1212 through C1217), FL1201, and FL1202 prevent the fundamental and sum frequencies of the high frequency and low frequency oscillators from appearing at the base of Q1203. The output of the filter network is the difference frequency signal between the high frequency oscillator and the low frequency oscillator.

During operation in the $0.2-$ to 1 -mc frequency range, the high frequency oscillator operates at 31 mc . The low frequency oscillator frequency is 28 mc ; therefore, the difference in frequency is 3 mc .

During operation in the 1 - to 2 -mc frequency range, the high frequency oscillator operates at 32 mc . The low frequency oscillator frequency is 28 mc ; therefore, the difference in frequency is 4 mc .

The output of the filters is applied to voltage amplifiers Q1202, Q1203, and Q1204 which amplify the signal. The signal is then applied to J1101 of the electronic package.

## 4-21. OPERATION IN THE 2- TO 7-MC TUNING RANGE

During operation in the 2 - to 7 -mc tuning range, the $17.5-\mathrm{mc}$ oscillator and the high frequency oscillator are operating, with the low frequency oscillator disabled. (See figures 4-4, 7-1, and 7-2.)

The $17.5-\mathrm{mc}$ signal is applied to J 1105 of the electronic package and then through Darlington amplifier A1202 to the base of transistor Q1201.

The high frequency output of A1201 and the 17.5mc output of A1202 are linearly mixed in the base circuit and then amplified by Q1201.

When the $17.5-\mathrm{mc}$ oscillator is operating, a B+ voltage is applied through C1105 and R1225 to the anode of CR1202. This positive voltage forward blases CR1202, shorting the output of C1207 to ground. The signal must therefore go through Q1202 and the filter network.

The output of Q1201 is rectified by CR1201 and applied to Q1202. Transistor Q1202 amplifies the signal to help overcome the loss in the following

## G133F HF RECEIVER CRYSTAL UTILIZATION

| RECEIVER <br> FREQUENCY RANGE IN MEGACYCLES | TURRET CRYSTAL |  | 17.5aMC OSCILLATOR | L-F CRYSTAL OSCILLATOR$(2 \times 14 M C=28 M C)$ |
| :---: | :---: | :---: | :---: | :---: |
|  | FREQUENCY (MC) | SYMBOL |  |  |
| 0.2 - 1.0 | 15.5 | Y20 | OFF | ON |
| 1.0-2.0 | 16.0 | Y12 | OFF | ON |
| 2.0 - 3.0 | 12.5 | Y1 | ON | OFF |
| 3.0 - 4.0 | 11.5 | Y2 | ON | OFF |
| 4.0-5.0 | 10.5 | Y3 | ON | OFF |
| $5.0 \cdot 6.0$ | 9.5 | Y4 | ON | OFF |
| $6.0 \cdot 7.0$ | 8.5 | Y5 | ON | OFF |
| 7.0-8.0 | 10.0 | Y6 | OFF | OFF |
| 8.0 - 9.0 | 11.0 | Y7 | OFF | OFF |
| 9.0 - 10.0 | 12.0 | Y8 | OFF | OFF |
| 10.0-11.0 | 13.0 | Y9 | OFF | OFF |
| 11.0-12.0 | 14.0 | Y10 | OFF | OFF |
| 12.0-13.0 | 15.0 | Y11 | OFF | OFF |
| 13.0-14.0 | 16.0 | Y12 | OFF | OFF |
| 14.0-15.0 | 8.5 | Y5 | OFF | OFF |
| 15.0-16.0 | 9.0 | Y13 | OFF | OFF |
| 16.0-17.0 | 9.5 | Y4 | OFF | OFF |
| 17.0-18.0 | 10.0 | Y6 | OFF | OFF |
| $18.0-19.0$ $190-20.0$ | 10.5 11.0 | $Y 6$ $Y 7$ | OFF | OFF |
| $19.0-20.0$ $20.0-21.0$ | 11.0 | $Y 7$ $Y 2$ | OFF | OFF |
| 21.0-22.0 | 12.0 | Y8 | OFF | OFF |
| 22.0-23.0 | 12.5 | Y1 | OFF | OFF |
| 23.0-24.0 | 13.0 | Y9 | OFF | OFF |
| 24.0-25.0 | 13.5 | Y18 | OFF | OFF |
| 25.0-26.0 | 14.0 | Y10 | OFF | OFF |
| 26.0-27.0 | 14.5 | Y19 | OFF | OFF |
| 27.0-28.0 | 15.0 | Y11 | OFF | OFF |
| 28.0-29.0 | 15.5 | Y20 | OFF | OFF |
| 29.0-30.0 | 16.0 | Y12 | OFF | OFF |

Table 4-1
filters. The LC filters FL1201 and FL1202 prevent the fundamental and sum frequencies of the high frequency oscillator and $17.5-\mathrm{mc}$ oscillator from appearing at the base of Q1203. The output of the filter network is the difference frequency signal between the high frequency oscillator and 17.5 mc .

As the frequency range of the receiver is changed from 2 to 7 mc , the high frequency crystal-controlled oscillator output signal will vary in $1-\mathrm{mc}$ steps from 12.5 to 8.5 mc , and the difference frequency will vary in the same manner from 5 to 9 mc .

FL1201 and FL1202 are notch filters which prevent some of the fundamental frequencies of the high frequency crystal-controlled oscillator ( $8.5 \mathrm{mc}, 9.5$ mc , and 10.5 mc ) from being passed on to the next stage.

The output of the filters is amplified by Q1203, Q1204, and Q1205, and applied to J1101 of the electronic package.

## 4-22. OPERATION IN THE 7-TO 30-MC TUNING RANGE

During operation in the 7 - to $30-\mathrm{mc}$ tuning range, both the low frequency crystal-controlled oscillator and the $17.5-\mathrm{mc}$ oscillator are disabled, and the high frequency crystal-controlled oscillator is operating. (See figures 4-5, 7-1, and 7-2.)

The output signal from the high frequency oscillator is applied to J1103 on the electronic package and then through Darlington amplifier A1201 to transistor Q1201.

The high frequency oscillator signal is amplified by Q1201 and coupled through C1206, C1207 and R1216, C1209 and R1219, C1211, and C1220 to the base of Q1203.

With the low frequency oscillator and the $17.5-\mathrm{mc}$ oscillator both inoperative, no B+ voltage is applied to C1105 or C1106. A negative voltage is applied to CR1202 back-biasing it, and the high frequency signal is allowed to pass on to Q1203, bypassing the filter network.

The high frequency oscillator signal is amplified by Q1203, Q1204, and Q1205, and applied to J1101 of the electronic package.

## 4-23. OPERATION OF THE VARIABLE FREQUENCY OSCILLATOR

The variable frequency oscillator is operating during operation of the G133F Receiver in all of its frequency ranges. The signal from the variable frequency oscillator is applied to jack J1106 of the electronic package and then through Darlington amplifier A1204 to J1102. The frequency of the oscillator is continuously variable from 2.5 mc to 3.5 mc .

## Note

V501 and V15 are one and the same. V502 and V18 are one and the same.






